

## Sheet No. 1

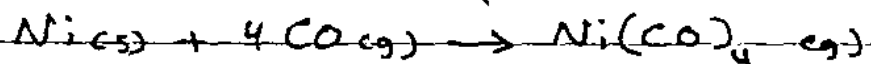
### molecular diffusion for Gas and liquids Tutorial

Q1 A small diameter tube closed at one end, was filled with acetone to within 18 mm of the top and maintained at 298 K and 99.75 kN/m<sup>2</sup> with a gentle stream of air blowing across the top. After about 15 Ksec the liquid level had fallen to 27.5 mm. Calculate the diffusivity of acetone in air?  $\rho_{\text{acetone}} = 790 \text{ kg/m}^3$   
 $\mu_{\text{air}} = 58$  and  $P_{\text{A}}^{\circ}(\text{acetone}) = 21.95 \text{ kN/m}^2$ .

Q2 Ammonia gas is diffusing at a constant rate through a layer of stagnant air 1 mm thick. Conditions are fixed so that the gas contains 50% by volume of ammonia at outer boundary of a stagnant layer. The ammonia diffusing to the other boundary is quickly absorbed and the concentration is negligible at that plane. The temp. is 295 K and pressure atmospheric, under these conditions the diffusivity of NH<sub>3</sub> in air is 0.18 cm<sup>2</sup>/sec. Calculate the rate of diffusion of ammonia through the layer?  
 $R = 8.314 \text{ J/mol} \cdot \text{K}$

Q3 Calculate the diffusivity of ethanol (C<sub>2</sub>H<sub>5</sub>OH) in air at 20°C and atmospheric pressure in m<sup>2</sup>/sec. Given that the atomic volumes  
 For Carbon = 0.014 m<sup>3</sup>/kgmol  
 For Oxygen = 0.0074  
 For H<sub>2</sub> = 0.0037  
 For air = 0.0299

Q4 Nickel Carbonyl (A) is produced by passing Carbon monoxide (B) at 323 K and 1 atm over a nickel slab. The following reaction takes place at the solid surface:-



The reaction is very rapid, so that the partial pressure of CO at the metal surface is essentially zero. The gases diffuse through a film 0.625 mm thick. At steady state, estimate the rate of production of nickel carbonyl in  $\text{mol/m}^2 \cdot \text{sec}$ . The composition of the bulk gas phase is 50% mol CO.  $D_{AB} = 20.0 \text{ mm}^2/\text{sec}$ .

Q5 By what percentage would the rate of mass transfer be increased or decreased by increasing the total pressure from  $[200 - 400] \text{ kN/m}^2$  in the following cases:-

1- The absorption of  $\text{SO}_2$  from  $\text{SO}_2$  air mixture containing 15% by volume  $\text{SO}_2$  using pure water as absorbing solvent.

2- The same as case (1), but the absorbing solvent contains amount of  $\text{SO}_2$  which exerts  $70 \text{ kN/m}^2$  partial pressure of  $\text{SO}_2$ .

Q1)  $z_1 = 18 \text{ mm} = 0.018 \text{ m}$   $z_2 = 0.0275 \text{ m}$   
 $T = 298 \text{ K}$   $P_T = 99.75 \text{ kN/m}^2$   $M.Wt = 58$   
 $t = 15 \text{ Ksec}$   $\rho_A = 790 \text{ kg/m}^3$   $P_A = 21.95 \text{ kN/m}^2$   
 Find  $D_{AB}$ ?

$$\frac{-D_{AB}}{R \cdot T} \cdot \frac{P_T}{P_{B1}} (P_{A2} - P_{A1}) \cdot \int dz = \frac{\rho_A}{M_A} \int dz \cdot z$$

$$\frac{-D_{AB}}{R \cdot T} \cdot \frac{P_T}{P_{B1}} (P_{A2} - P_{A1}) \cdot t = \frac{\rho_A}{M_A} \cdot \left( \frac{z_2^2}{2} - \frac{z_1^2}{2} \right)$$

$$P_{A1} = P_A^0 = 21.95 \text{ kN/m}^2 \quad P_{A2} = 0$$

$$P_{B1} = P_T - P_{A1}$$

$$= 99.75 - 21.95 = 77.8 \text{ kN/m}^2 \quad P_{B2} = 99.75 \text{ kN/m}^2$$

$$\therefore P_{B1} = \frac{P_{B2} - P_{B1}}{\ln \frac{P_{B2}}{P_{B1}}} = \frac{99.75 - 77.8}{\ln \frac{99.75}{77.8}} = 85.33 \text{ kN/m}^2$$

$$\therefore \frac{-D_{AB}}{(8.314)(298)} \cdot \frac{99.75}{85.33} (0 - 21.95) (15 \times 1000) = \frac{790}{58} \left( \frac{0.0275^2}{2} - \frac{0.018^2}{2} \right)$$

$$\therefore D_{AB} = 1.9 \times 10^{-5} \text{ m}^2/\text{sec}$$

$$\frac{\text{kmol} \cdot \text{m}^2}{\text{m}^2 \cdot \text{sec}} \cdot \frac{\text{KJ}}{\text{kmol} \cdot \text{K}} \cdot \text{K} = \frac{\text{KJ}}{\text{m}^2 \cdot \text{kg}} \cdot \frac{\text{kg}}{\text{m}^3} \cdot \text{m}^2$$

Q2

$$Z = 1 \text{ mm} = 0.01 \text{ cm}$$

$$y_{A1} = 0.5 \quad T = 295 \text{ K} \quad P_T = 1 \text{ atm}$$

$$D_{AB} = 0.18 \text{ cm}^2/\text{s} \quad \text{find } N_A ?$$

For stagnant layer:-

$$N_A = \frac{-D_{AB}}{R \cdot T} \cdot \frac{1}{Z} \cdot \frac{P_T}{P_{BM}} \cdot (P_{A2} - P_{A1})$$

$$\frac{-0.18 \times 10^{-4}}{(8.314)(295)} \cdot \frac{1}{0.001} \cdot \frac{101.3}{P_{BM}} (P_{A2} - P_{A1})$$

$$P_{A1} = y_{A1} \cdot P_T = 0.5 \times 101.3 = 50.65 \text{ kN/m}^2$$

$$P_{A2} = y_{A2} \cdot P_T = \text{Zero} \quad (\text{quickly absorbed})$$

$$\left. \begin{aligned} P_{B1} &= 101.3 - 50.65 = 50.65 \text{ kN/m}^2 \\ P_{B2} &= 101.3 - \text{Zero} = 101.3 \text{ kN/m}^2 \end{aligned} \right\} P_{BM} = \frac{P_{B2} - P_{B1}}{\ln \frac{P_{B2}}{P_{B1}}}$$

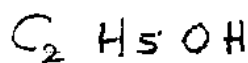
$$\therefore P_{BM} = 73.07 \text{ kN/m}^2$$

$$\therefore \frac{-7.43 \times 10^{-4} \cdot (0 - 50.65)}{73.07} = N_A$$

$$N_A = 5.153 \times 10^{-4} \text{ kmol/m}^2 \cdot \text{s}$$

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Q3

find  $D_{AB}$ ?

$$D_{AB} = \frac{b \cdot T^{3/2}}{P_T (U_A^{1/3} + U_B^{1/3})^2} \cdot \left( \frac{1}{M_A} + \frac{1}{M_B} \right)^{0.5}$$

To find  $U_A, U_B$  :-

$$U_A = \sum U_i$$

$$= U_{O_2} + U_H + U_C$$

$$U_C = 2 \times 0.14 = 0.029 \text{ m}^3/\text{kmol}$$

$$U_H = 6 \times 0.0037 = 0.022$$

$$U_{O_2} = 0.0074 / 2 = 3.7 \times 10^{-3} \text{ s (atomic)}$$

$$\therefore U_A = 0.029 + 0.022 + 3.7 \times 10^{-3}$$

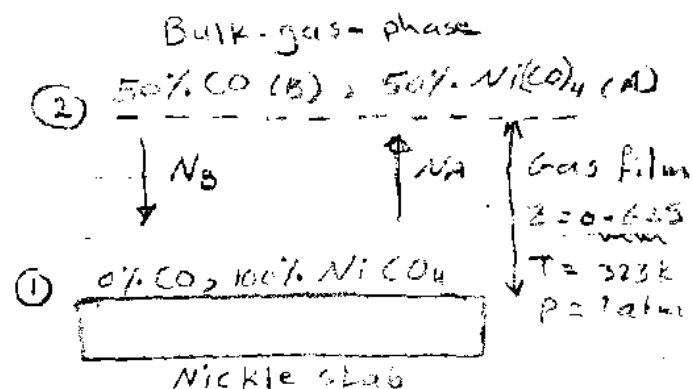
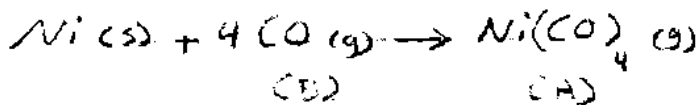
$$U_A = 0.055 \text{ m}^3/\text{kmol}$$

$$\therefore D_{AB} = \frac{(0.004)(293)}{101.3 \times (0.055^{1/2} + 0.0297^{1/2})^2} \cdot \left( \frac{1}{46} + \frac{1}{29} \right)^{0.5}$$

$$D_{AB} = \frac{1.172}{49.35} (0.234)$$

$$D_{AB} = 5.63 \times 10^{-3} \text{ kmol/m}^2 \cdot \text{s}$$

Q4



From stoichiometry:-

$$N_B = -4 N_A \quad N_T = N_A + N_B = N_A - 4 N_A = -3 N_A$$

$$N_A = -D_{AB} \cdot C_T \cdot \frac{dy_A}{dz} + y_A (N_A + N_B)$$

$$\therefore N_A = \frac{N_A}{(N_A + N_B)} \cdot \frac{D_{AB} \cdot C_T}{z} \ln \left[ \frac{\left( \frac{N_A}{N_A + N_B} \right) - y_{A2}}{\left( \frac{N_A}{N_A + N_B} \right) - y_{A1}} \right]$$

$$\frac{N_A}{N_A + N_B} = -\frac{1}{3}$$

$$\therefore N_A = \frac{-1}{3} \cdot \frac{D_{AB}}{R \cdot T} \cdot \frac{P_T}{z} \ln \left[ \frac{-\frac{1}{3} - y_{A2}}{-\frac{1}{3} - y_{A1}} \right]$$

$$y_{A1} = 1.0 \quad y_{A2} = 0.5$$

$$\therefore N_A = \frac{(2.0 \times 10^{-5} \text{ m}^2/\text{s}) (1.013 \times 10^5 \text{ Pa})}{3 \times (8.13) (323) (0.625 \times 10^{-3})} \ln \left( \frac{1/3 + 1.0}{1/3 + 0.5} \right)$$

$$N_A = 0.187 \text{ mol / m}^2 \cdot \text{s}$$

separating the variables:-

$$\frac{-dy_A}{N_A - y_A (N_A + N_B)} = \frac{dz}{C_T D_{AB}}$$

Q5

Case (1)

$$P_T = 200 \text{ kN/m}^2$$

$$N_A = - \frac{D_{AB}}{R.T.Z} \cdot \frac{P_T}{P_{BM}} (P_{A2} - P_{A1})$$

$$P_{A1} = 0 \quad P_{A2} = \gamma \cdot z \cdot P_T = 0.15 \times 200 = 30 \text{ kN/m}^2$$

$$P_{BM} = \frac{P_{A1} - P_{A2}}{\ln \frac{P_T - P_{A2}}{P_T - P_{A1}}} = \frac{0 - 30}{\ln \frac{200 - 30}{200 - 0}} = 184.6 \text{ kN/m}^2$$

$$N_A = - 32.5 \frac{D_{AB}}{R.T.Z} = - 32.5 A$$

$$\text{When } P_T = 400 \quad \text{then } P_{A2} = 0.15 \times 400 = 60 \text{ kN/m}^2$$

$$P_{BM} = 369.2 \text{ kN/m}^2$$

$$\frac{D_{200}}{D_{400}} = \frac{400}{200} = 2 \quad \therefore D_{AB} \Big|_{400} = \frac{1}{2} D_{AB} \Big|_{200}$$

$$\therefore N_A = - \frac{D_{AB}}{2 R.T.Z} \cdot \frac{400}{369.2} \times 60 = - 32.5 \frac{D_{AB}}{R.T.Z}$$

$\therefore$  No change in  $N_A$

Case (2)

$$P_T = 200 \text{ kN/m}^2$$

$$P_{A1} = 10 \text{ kN/m}^2$$

$$P_{A2} = 30 \text{ kN/m}^2$$

$$\therefore P_{BM} = \frac{10 - 30}{\ln \frac{200 - 30}{200 - 10}} = 179.8 \text{ kN/m}^2$$

$$\therefore N_A = - \frac{D_{AB}}{R.T.Z} \cdot \frac{200}{179.8} (30 - 10) \Rightarrow - 22.25 \frac{D_{AB}}{R.T.Z}$$

increasing  $(P)$  to be  $(400 \text{ kN/m}^2)$

$$P_T = 400 \text{ kN/m}^2 \quad P_{A1} = 10 \text{ kN/m}^2 \quad P_{A2} = 60 \text{ kN/m}^2$$

$$P_{BM} = 364.4 \text{ kN/m}^2$$

$$N_A = - \frac{D_{AB}}{R.T.Z} \cdot \frac{400}{364.4} (60 - 10) = - 22.44 \frac{D_{AB}}{R.T.Z}$$

Q6 Two Large vessels are connected as in figure.  
Vessel (1) contains 80%  $N_2$  (A) and 20%  $O_2$  (B).

Vessel (2) contains 20%  $N_2$  and 80%  $O_2$ .

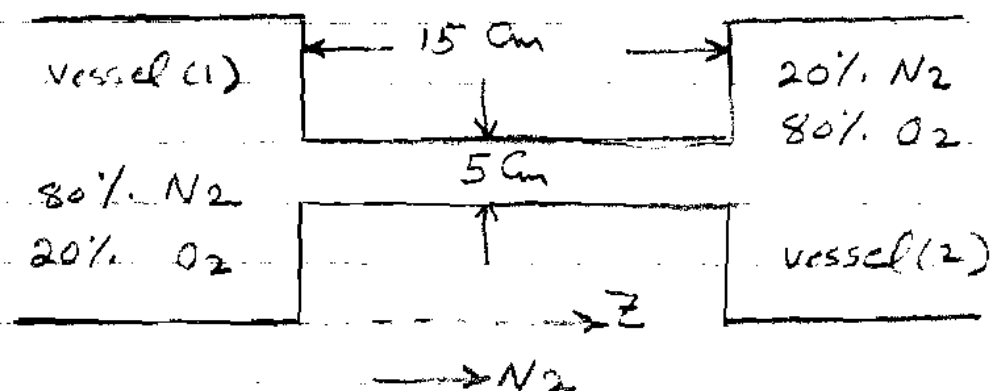
The temp.  $20^\circ C$  and total pressure (2 atm). Calculate:

1. The flux and rate of transport of ( $N_2$ ) from vessel (1) to vessel (2), and same for ( $O_2$ ).

2. The partial pressure of ( $N_2$ ) and its gradient in the tube (0.05 m) from vessel (1).

3. The net mass flux ( $n_T$ ).

Given that  $D_{AB} = 1.01 \times 10^{-5} \text{ m}^2/\text{sec}$ .





For EMD :-

$$a) N_A = \frac{-D_{AB}}{R \cdot T} \cdot \frac{1}{z_2 - z_1} (P_{A1} - P_{A2})$$

$$P_{A1} = y_{A1} \cdot P_T$$

$$= 0.8 \times 2$$

$$= 1.6 \text{ atm}$$

$$P_{A2} = y_{A2} \cdot P_T$$

$$= 0.2 \times 2$$

$$= 0.4 \text{ atm}$$

$$z_2 - z_1 = 0.15 \text{ m}$$

$$\therefore N_A = 3.36 \times 10^{-6} \text{ kmol/m}^2 \cdot \text{s}$$

$$N_B = -N_A = -3.36 \times 10^{-6} \text{ kmol/m}^2 \cdot \text{s}$$

$$N_A = N_A \times \text{Area} = 3.36 \times 10^{-6} \times \frac{\pi}{4} (0.05)^2$$

$$N_A = 6.6 \times 10^{-9} \text{ kmol/sec.}$$

$$b) \frac{dP}{dz} = \frac{P_{A2} - P_{A1}}{z} = \frac{0.4 - 1.6}{0.15} = -8 \text{ atm/m}$$

at point 0.05

$$P_A = P_{A1} + \frac{dP}{dz} \cdot \Delta z$$

$$= 1.6 + (-8) \cdot 0.05$$

$$= 1.2 \text{ atm}$$

$$c) N_T = N_A \cdot Mwt_A + N_B \cdot Mwt_B$$

$$= (3.36 \times 10^{-6} \times 28) - (3.36 \times 10^{-6} \times 32)$$

$$= -1.344 \times 10^{-5} \text{ kmol/m}^2 \cdot \text{s}$$

multiply by  $(V_A)$

$$V_A = \frac{V_A}{V_A + V_B} \cdot \frac{C \cdot D_{AD}}{2} \ln \left[ \frac{\frac{V_A}{V_A + V_B} - \gamma_{A2}}{\frac{V_A}{V_A + V_B} - \gamma_{A1}} \right]$$