



Theory of Structures (I) - BCE
Third Year

May 29, 2016
Final Exam – First Attempt

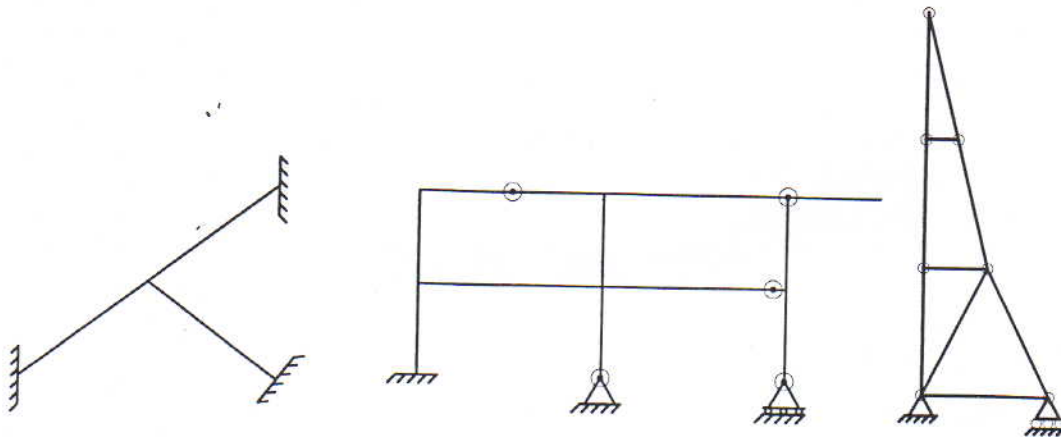
Time: 3 Hours
Closed Book & Notes

Answer 4 questions only.

ثالث انشائية

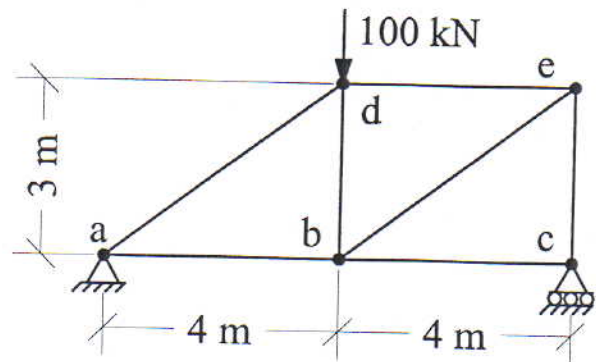
Q1:

- Write briefly about the structural analysis and design; discuss safety, economy and serviceability for the structures and the main role of engineer to provide these requirements.
- Sometimes it is important to use an inactive members in a truss, define inactive these members and why it should be used for?
- What is the stiffness and flexibility mean for structural engineer?
- Discuss the stability and determinacy of the 3 structures shown:



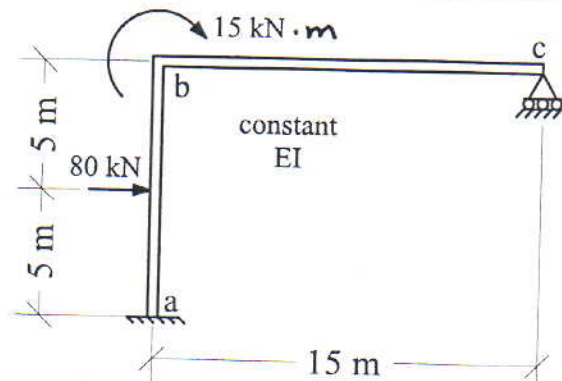
Q2:

For the structural truss shown, using the Unit Load Method, find the vertical deflection of joint B in terms of EA. EA = constant for all members.



Q3:

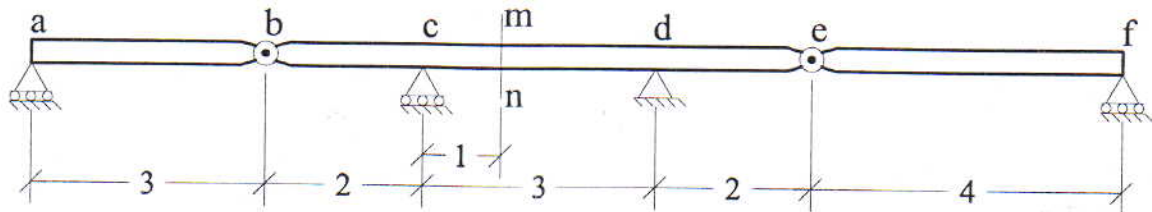
For the structural frame shown, using the Consistent Deformation Method, draw the bending moment diagram for member bc.





Q4:

- For the structural beam shown below, draw the influence line for: R_a ; R_c ; M_c ; M_d ; $V_{c_{right}}$; M_{mn} ; V_{mn} ; $V_{d_{left}}$ and V_e .
- Find the value of M_{mn} if the structural beam is subjected to infinite uniformly distributed load ($w = 30 \text{ kN/m}$).

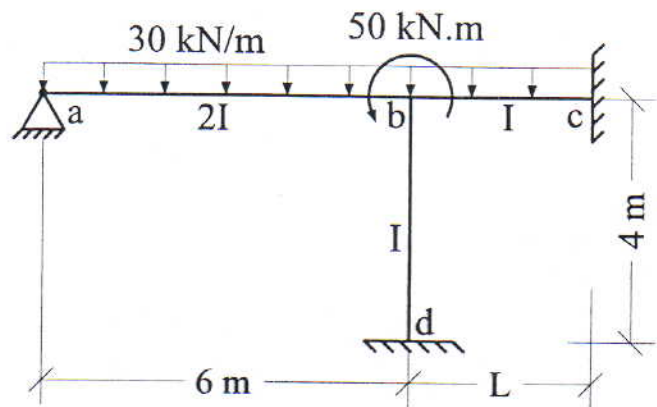


Q5:

For the structural frame shown, use the Slope Deflection Method; find the span length (L) such that the rotation at joint (b) will not exceed 4.22° (in counterclockwise). The frame members have a modulus of elasticity (E) = $2 \times 10^5 \text{ N/mm}^2$ and the moment of inertia (I) = $30 \times 10^5 \text{ mm}^4$.

Notes:

- $\pi \text{ rad.} / 180^\circ = 1$.
- The fixed end moments (FEM) for the uniformly distributed load at the member ends equal $\pm w\ell^2/12$.
- Use iteration method to solve the equation, start with $L = 1 \text{ m}$, $L \leq 3 \text{ m}$.

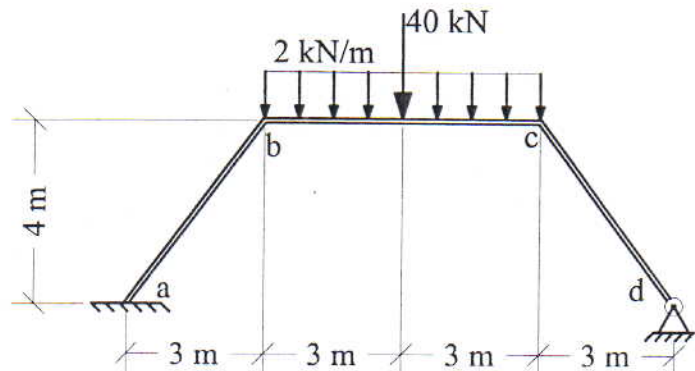


Q6:

Using the Moment Distribution Method, find the reactions at support a (a_x & a_y) due to the applied loading shown. $EI = \text{constant}$. If it needed, try up to three cycles only.

Notes:

- The fixed end moments (FEM) for the uniformly distributed load at the member ends equal $\pm w\ell^2/12$.
- The fixed end moments (FEM) for the midspan concentrated load at the member ends equal $\pm p\ell/8$.

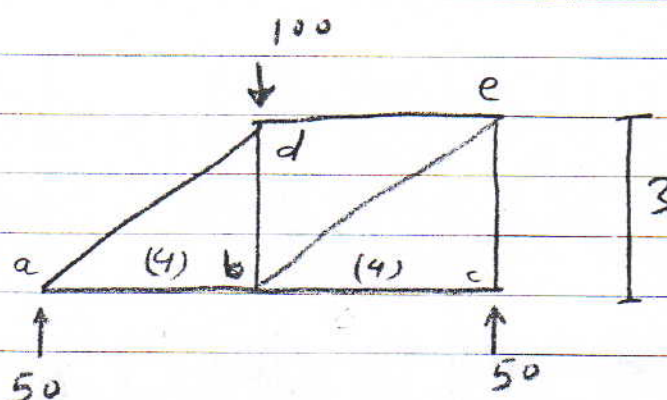


Good Luck

Final Exam - First Attempt, 2016 - Solution:

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Q2:

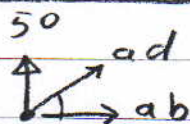


mem	L/EA	$S (kN)$	u	SuL/EA
ab	$4/EA$	$+66.67$	0.667	$1600/9 EA$
bc	$4/EA$	0	0	0
ad	$5/EA$	-83.33	-0.833	$3125/9 EA$
de	$4/EA$	-66.67	-0.667	$1600/9 EA$
be	$5/EA$	83.33	0.833	$3125/9 EA$
ce	$3/EA$	-50	-0.5	$75/EA$
bd	$3/EA$	-50	0.5	$-75/EA$

$$\therefore \sum \frac{SuL}{EA}$$

$$= \frac{1050}{EA} = \Delta_b$$

Σ: ⊗ joint a:

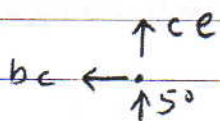


$$\theta = \arctan(3/4) = 36.87^\circ \quad \sum F_y = 0 \Rightarrow 50 + ad \sin \theta = 0$$

$$ad = -83.33 \text{ kN}$$

$$\sum F_x = 0 \Rightarrow ad \cos \theta + ab = 0 \Rightarrow ab = +66.67 \text{ kN}$$

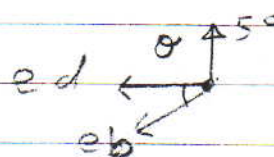
⊗ joint c:



$$\Rightarrow \sum F_x = 0 \Rightarrow bc = 0 \text{ and } \sum F_y = 0$$

$$ce = -50 \text{ kN}$$

⊗ joint e:

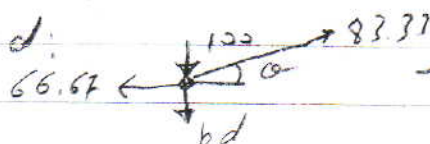


$$\sum F_y = 0 \Rightarrow 50 = eb \sin \theta$$

$$eb = 83.33 \text{ kN}$$

$$\sum F_x = 0 \Rightarrow ed + eb \cos \theta = 0 \Rightarrow ed = -66.67$$

⊗ joint d:

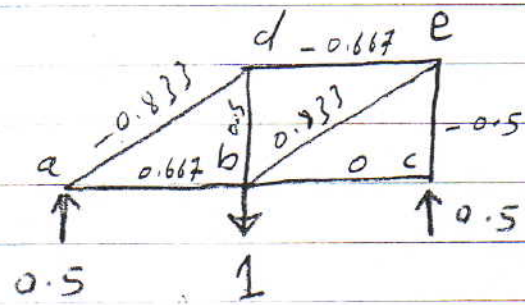


$$\sum F_y = 0 \Rightarrow 100 + bd = 83.33 \sin \theta$$

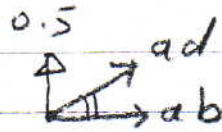
$$bd = -50 \text{ kN}$$

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Joint a:

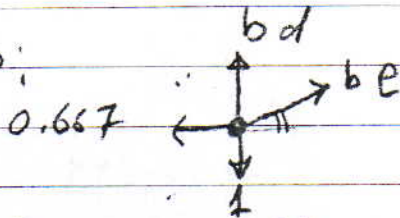


$$\sum F_y = 0$$

$$0.5 + ad \sin \theta = 0 \Rightarrow ad = -0.833$$

$$\sum F_x = 0 \Rightarrow +0.833 \cos \theta = ab \Rightarrow ab = 0.6667$$

Joint b:

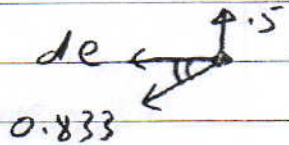


$$\sum F_x = 0 \Rightarrow be \cos \theta = 0.667$$

$$be = 0.833$$

$$\sum F_y = 0 \Rightarrow 1 = 0.833 \sin \theta + bd \Rightarrow bd = +0.5$$

Joint e:



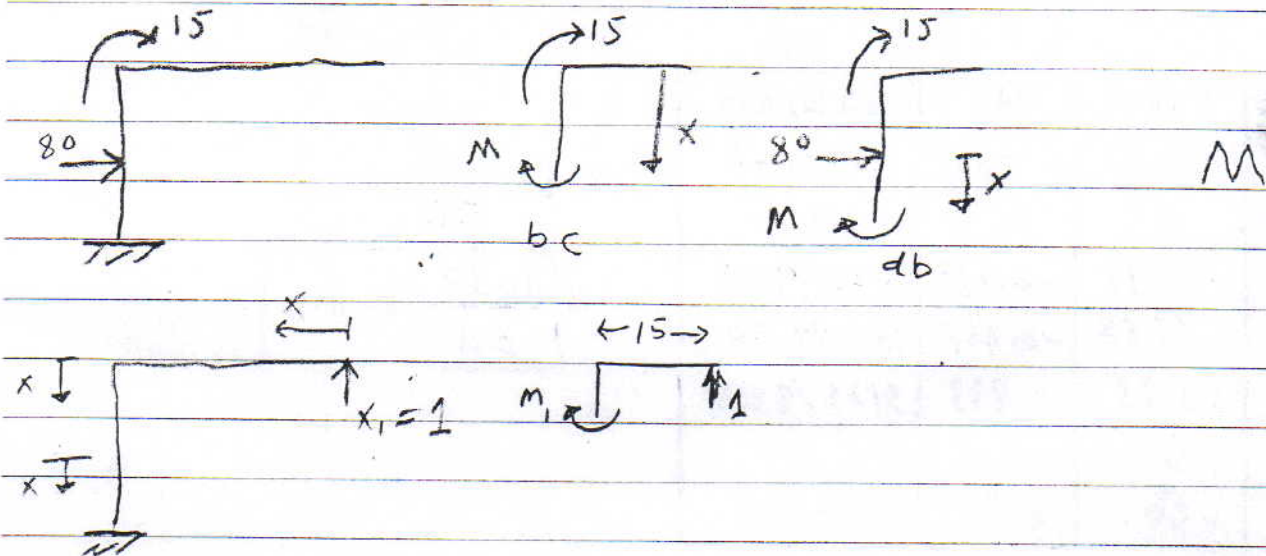
$$\sum F_x = 0 \Rightarrow 0.833 \cos \theta = -de$$

$$\therefore de = -0.667$$

Q3:

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membr	EI	orig.	limit	M	m_1	Mm_1	m_1^2
ab	1	b	0-5	$-15 - 80x$	x	$-15x - 80x^2$	x^2
bc	1	c	0-5	-15	15	-225	225
cd	1	d	0-15	0	15	0	225



$$\Delta_1 = \Delta_1' + \delta_{11} X_1$$

$$\Delta_1' = \int \frac{M m_1 dx}{EI} = \left[\int_0^5 (-15x - 80x^2) dx + \int_0^5 (-225) dx + 0 \right] \frac{1}{EI}$$

$$\Delta_1' = \frac{1}{EI} [-3520.833 - 1275] = \frac{-27875}{6EI} = -4645.833/EI$$

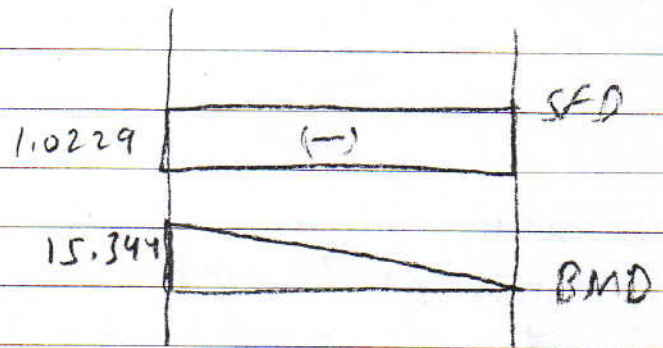
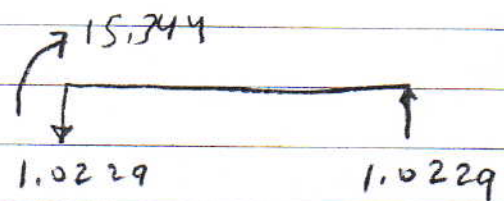
$$\delta_{11} = \int \frac{m_1 m_1 dx}{EI} = \left[\int_0^5 (x^2 + 225) dx + \int_0^{15} (225) dx \right] \frac{1}{EI}$$

$$= \frac{13625}{3EI} = 4541.666/EI$$

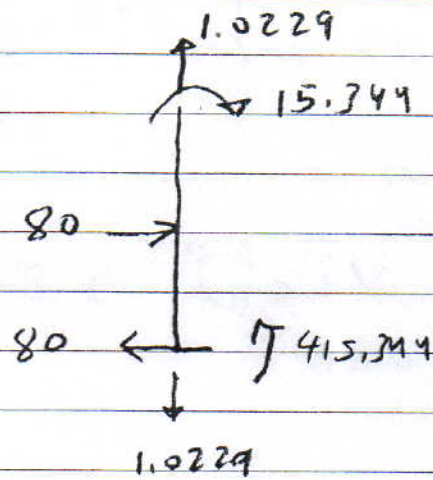
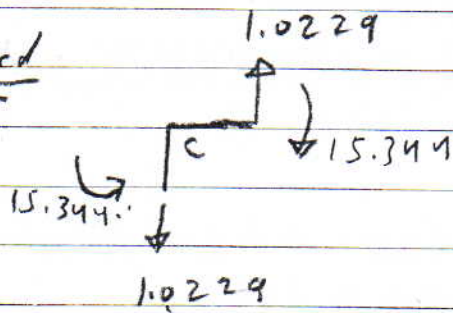
$$\therefore \frac{13625}{3EI} X_1 = \frac{27875}{6EI} \Rightarrow X_1 = 1.0229 \text{ kN } \uparrow$$

member cd

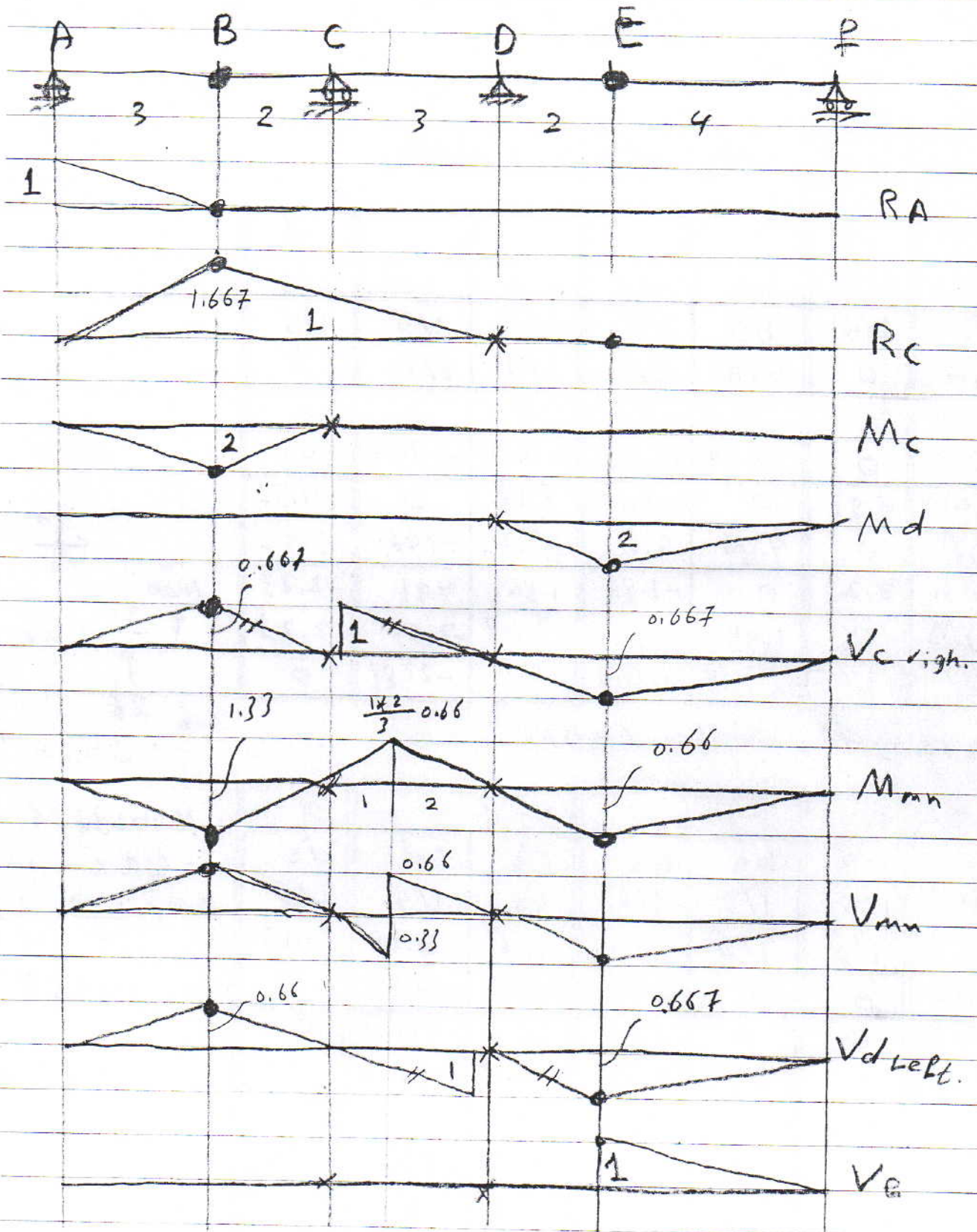
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not required



Q4

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$$M_{mn} = 30 \frac{\text{kN}}{\text{m}} \left[\frac{-1.33 \times 5}{2} + \frac{0.667 \times 3}{2} - \frac{0.667 \times 6}{2} \right] = -130 \text{ kN.m}$$

Q5:

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$$FEM_{ab} = \frac{-wL^2}{12} = \frac{-30 \times 6^2}{12} = -90$$

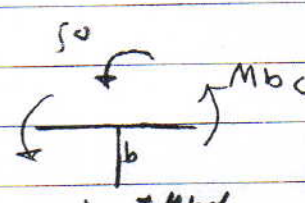
$$\theta_b = -4.22 D_{eq} \times \frac{\pi \text{ rad}}{180 \text{ Deg}} = -0.07365 \text{ rad.}$$

$$EI = 2 \times 10^5 \frac{\text{N}}{\text{mm}^2} \times 30 \times 10^5 \text{ mm}^4 = 6 \times 10^{11} \text{ N} \cdot \text{mm}^2 \times \frac{\text{kN}}{1000 \text{ mm}} \times \frac{\text{m}^2}{(1000)^2 \text{ mm}^2}$$

$$EI = 600 \text{ kN} \cdot \text{m}^2$$

$$\sum M_a = 0 \Rightarrow M_{ab} = 0 \Rightarrow \frac{2 \times 600}{6} [4\theta_a - 2(0.07365)] - 90 = 0$$

$$\therefore \theta_a = 0.1493 \text{ rad.}$$

$$\sum M_b = 0 \Rightarrow M_{ba} + M_{bd} + M_{bc} + 50 = 0$$


$$\frac{2 \times 600}{6} [2\theta_a - 4\theta_b] + 90 + \frac{600}{4} [-4\theta_b] + \frac{600}{L} [-4\theta_b] - \frac{30L^2}{12} = -50$$

$$\left(\frac{176.767}{L} + 2.5L^2 = 96.6165 \right) ; \frac{176.767}{L} + 2.5L^2 = R$$

L	R / 96.6165	$\therefore L = 2.05 \text{ m}$ ($L_{\text{exact}} = 2.0537 \text{ m}$)
1	1.855	
2	1.018288	
2.1	0.9853	
2.05	1.0012 ←	

Q 6: $FEM = F \left(\frac{WP^2}{12} + \frac{Pl}{8} \right) = F \left(\frac{2 \times 6^2}{12} + \frac{40 \times 6}{8} \right)$

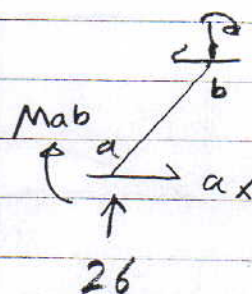
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$= F 36$

either:

1 - not using the modified MDM:

J	a	b		c		d
m	ab	ba	bc	cb	cd	dc
K	1/5	1/5	1/6	1/6	1/5	1/5
DF	0	6/11	5/11	5/11	6/11	1
FEM	0	0	-36	36	0	0
DM	0	19.64	16.36	-16.36	-19.64	0
COM	9.82	0	-8.18	8.18	0	-9.82
DM	0	4.46	3.72	-3.72	-4.46	9.82
COM	2.23	0	-1.86	1.86	4.91	-2.23
DM	0	1.01	0.85	-3.08	-3.69	2.23
Σ	12.05	25.11	-25.11	22.88	-22.88	0



or
2 - using the modified MDM

J	a	b		c		d
m	ab	ba	bc	cb	cd	dc
K	1/5	1/5	1/6	1/6	1/5	1/5
K'	1/5	1/5	1/6	1/6	0.15	0.15
DF	0	6/11	5/11	0.526	0.474	1
FEM	0	0	-36	36	0	0
DM	0	19.64	16.36	-18.936	-17.064	0
COM	9.82	0	-9.468	8.18	0	X
DM	0	5.16	4.3	-4.3	-3.88	
COM	2.58	0	-2.15	2.15	0	
DM	0	1.17	0.98	-1.13	-1.02	
Σ	12.4	25.97	-25.97	21.96	-21.96	0

$\Sigma M \text{ at } b = 0$

$M_{ab} + 3 \times 26$
 $= 4 a_x$

$\therefore a_x = \frac{M_{ab}}{4} + 19.5$

$a_{x1} = 22.5 \uparrow$

$a_{x2} = 22.6 \uparrow$