



UNIVERSITY OF TECHNOLOGY
Building and Construction Engineering Department
Final Exam. 1st attempt, 2014/2015
Subject : Sanitary Engineering
Branch : Building & Construction
Management Engineering Branch
Instructor: Ammar A. Al-Sultan



Class: 3rd Year
Time : 3 Hours

Date : May 31st , 2015

Note : Answer of FOUR questions

Q	Description	Score %
1-A	Differentiate (with drawings) between: 1- Sedimentation process & Filtration process in WTP. 2- Loop water network system & Tree water network system. 3- Lining system for Hazardous waste landfill (option -1) & lining system for Non-Hazardous biodegradable waste landfill.	15
1-B	Draw with full details the following items: 1- Typical leachate collection and removal system in landfill site. 2- Diagrammatic section of a rapid sand filter.	10
2-A	The two filters bed system as shown in fig (1), use Kawamura's formula to determine the followings: 1- The particle sizes of anthracite & ilmenite which have velocities equal to that sand 0.5mm in diameter. 2- The filter ratio (%) after increased the length of filter number 2, if the ($Q_{bw1} = 0.03 \times Q_1$), ($Q_{bw2} = 1.3 \times Q_{bw1}$) & ($Q_{bw2} = 0.025 \times Q_2$).	15
2-B	Explain with all definitions of the selected items in the fig (2).	10
3	A WTP contains the flocculation package system as shown in fig (3), this package divided by two basins, each one contain three equal zones & the overall detention time for each basin is 30 min, calculate: 1- The input flowrate in (m^3/d). 2- The concentration of Alum in (mg/l) if the quantity of coagulant is 120 kg/d. 3- The surface area for each basin & overall surface area. Use: $GT = 1 \times 10^5$, basin depth = 3.5 m, $\mu = 1.3 \times 10^{-3}$ kg/m.s	25
4	The sewer network including construction of the sewer pipe as shown in the fig (4), the trench of this pipe must be filling back by damp clay soil & it's intersect by 1.0 m inclined water channel that carry out loading of 1500 kg/m. Suggest a construction method at the intersection region according to ASTM specifications, use the following data in the fig (4).	25
5	Calculate the number of population in the residential area which receiving the portable water by pipeline AB, use the Monogram chart method and check the velocity in the pipeline AB as shown in the fig (5).	25

With my best wishes for success

10

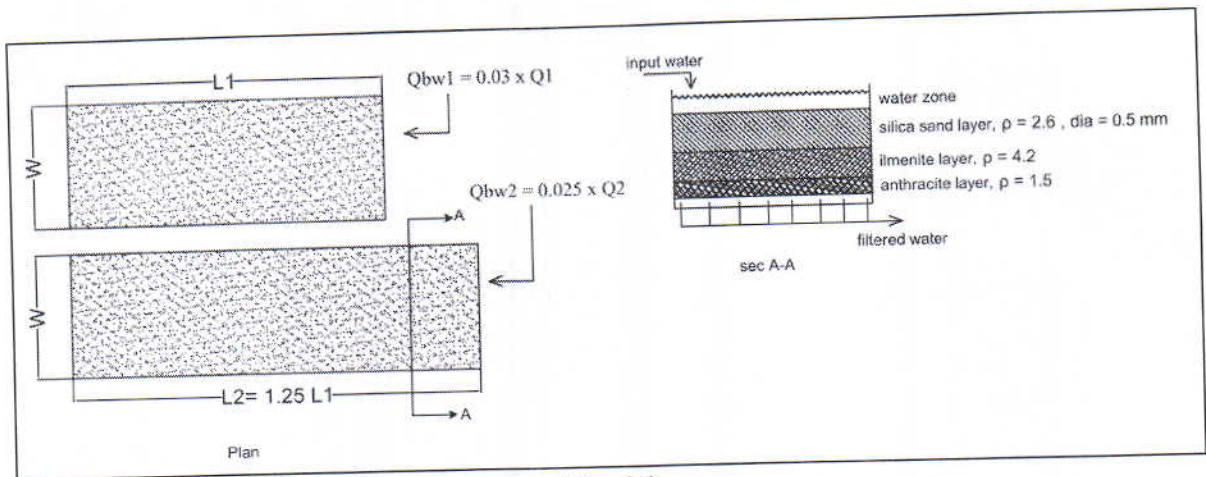


Fig (1)

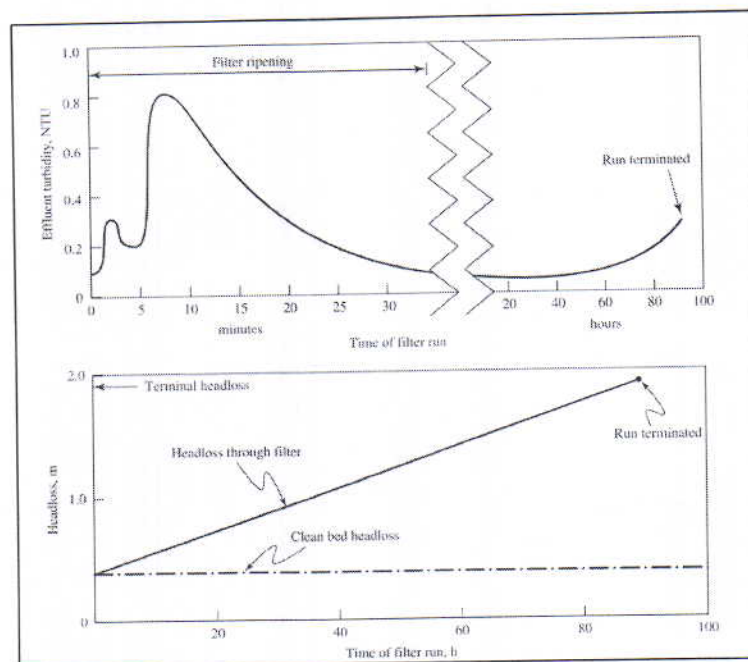


Fig (2)

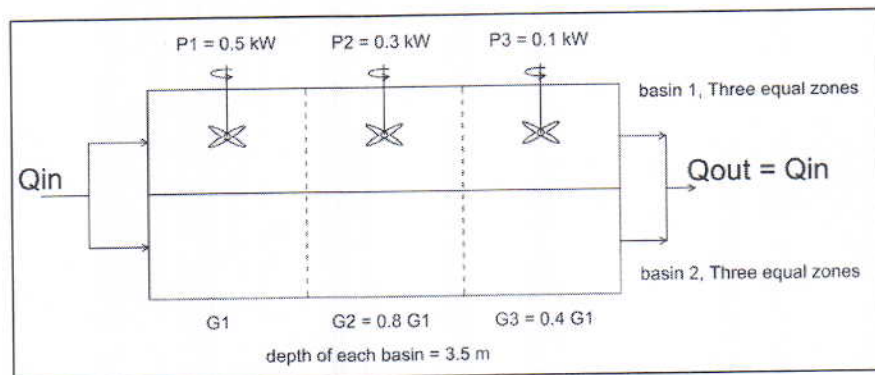


Fig (3)

8
2

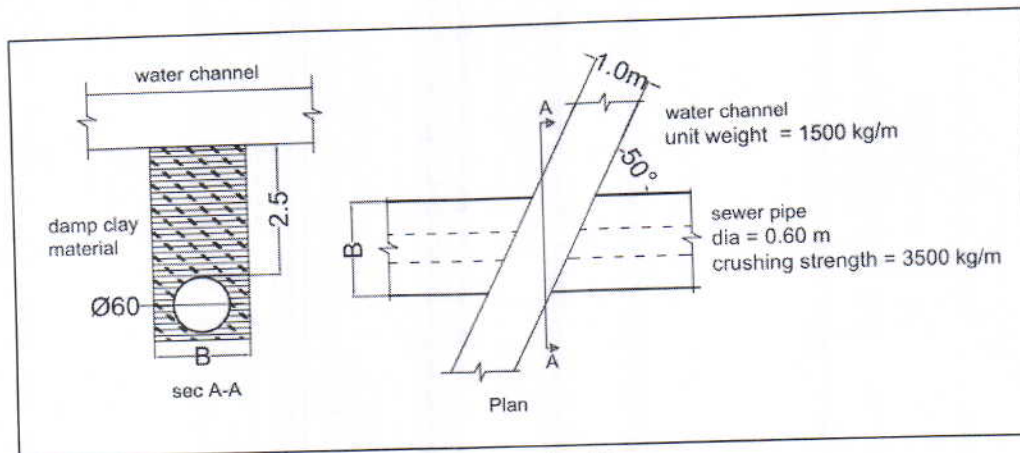


Fig (4)

Materials	Unit wt (kg/m ³)
Dry sand	1600
Ordinary sand	1840
Wet sand	1920
damp clay	1920
Saturated clay	2080
Saturated top soil	1840
Sand & damp top soil	1600

Soil type	Max value of ($k\mu$)
Cohesion less granular material	0.192
Sand & gravel	0.165
Sat. top soil	0.15
Clay	0.13
Sat. clay (wet clay)	0.11

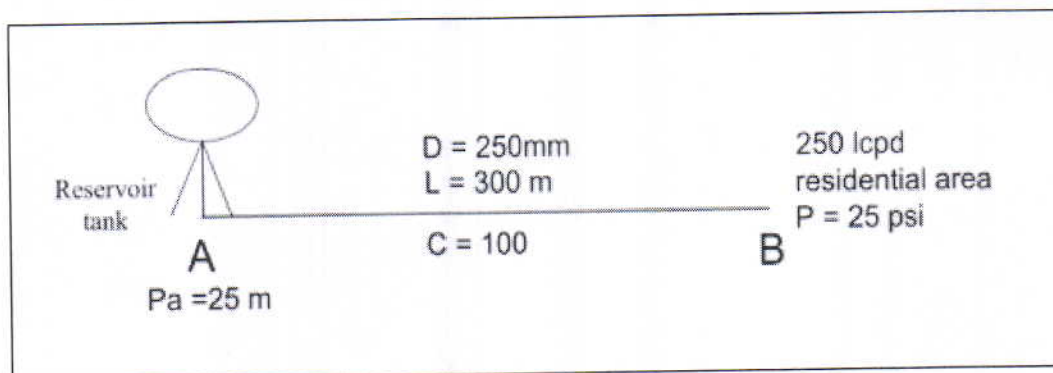


Fig (5)

8-2

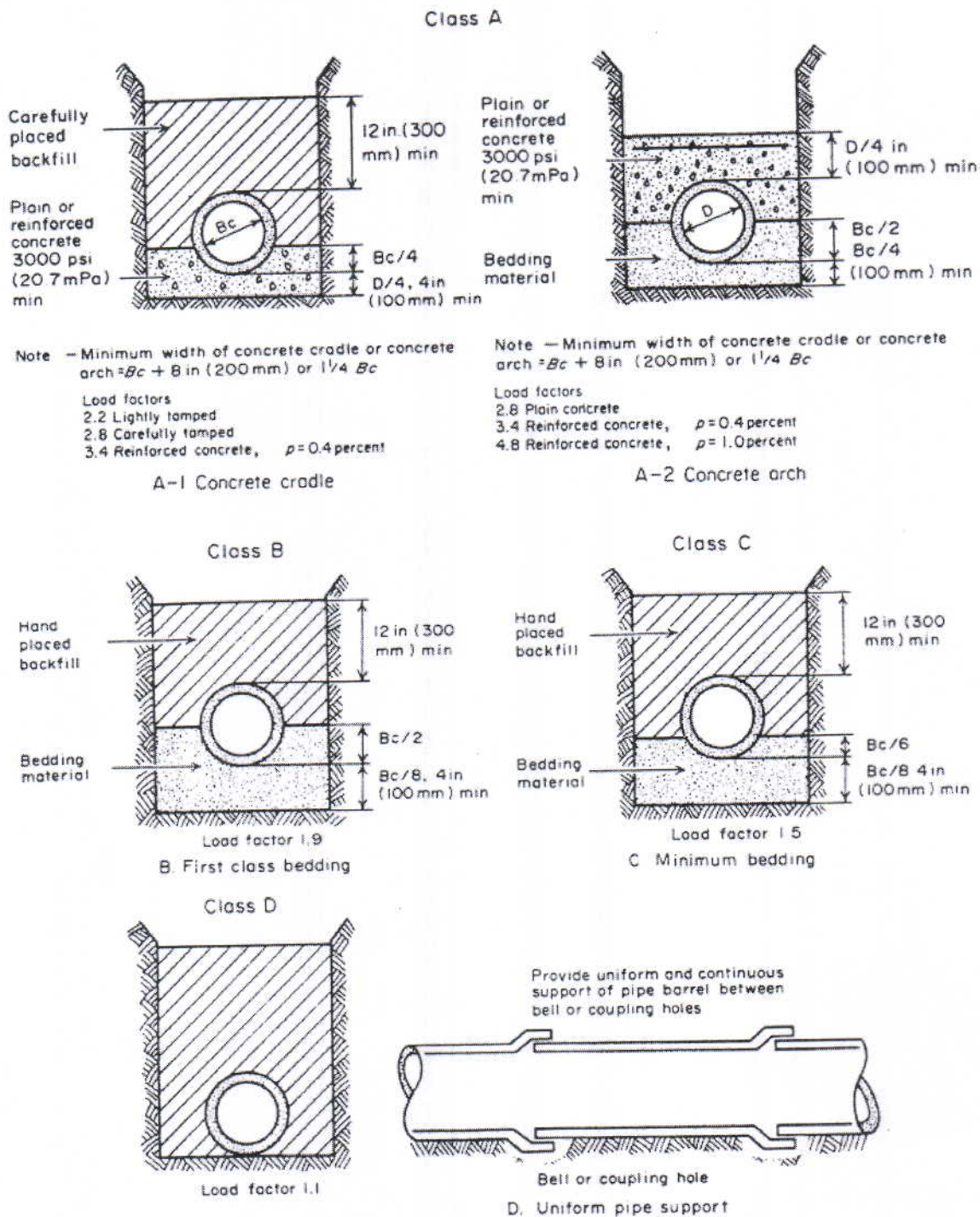


Figure 14-2 Methods of bedding clay pipe and load factors applicable to strength.⁴ (Reprinted by Permission of the American Society for Testing and Materials, Copyright 1977.)

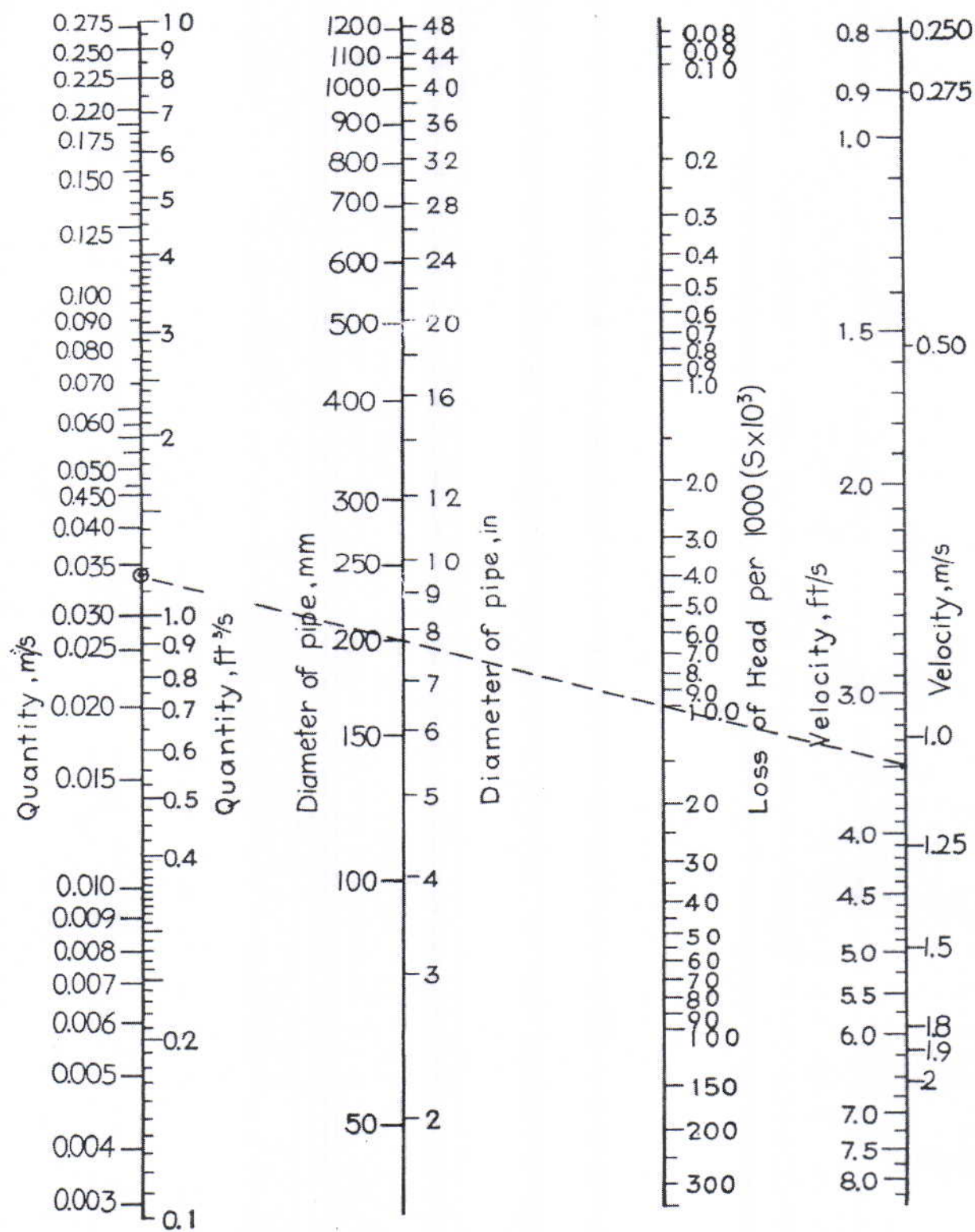


Figure 6-8 Flow in old cast-iron pipes. (Hazen-Williams $C = 100$.)

Table 14-5 Proportion of "long" superficial loads reaching pipe in trenches

Ratio of depth to width	Sand and damp topsoil	Saturated topsoil	Damp yellow clay	Saturated yellow clay
0.0	1.00	1.00	1.00	1.00
0.5	0.85	0.86	0.88	0.89
1.0	0.72	0.75	0.77	0.80
1.5	0.61	0.64	0.67	0.72
2.0	0.52	0.55	0.59	0.64
2.5	0.44	0.48	0.52	0.57
3.0	0.37	0.41	0.45	0.51
4.0	0.27	0.31	0.35	0.41
5.0	0.19	0.23	0.27	0.33
6.0	0.14	0.17	0.20	0.26
8.0	0.07	0.09	0.12	0.17
10.0	0.04	0.05	0.07	0.11

Table 14-6 Proportion of "short" superficial loads reaching pipe in trenches

Ratio of depth to width	Sand and damp topsoil		Saturated topsoil		Damp clay		Saturated clay	
	Max	Min	Max	Min	Max	Min	Max	Min
0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
0.5	0.77	0.12	0.78	0.13	0.79	0.13	0.81	0.13
1.0	0.59	0.02	0.61	0.02	0.63	0.02	0.66	0.02
1.5	0.46	0.48	0.51	0.54
2.0	0.35	0.38	0.40	0.44
2.5	0.27	0.29	0.32	0.35
3.0	0.21	0.23	0.25	0.29
4.0	0.12	0.14	0.16	0.19
5.0	0.07	0.09	0.10	0.13
6.0	0.04	0.05	0.06	0.08
8.0	0.02	0.02	0.03	0.04
10.0	0.01	0.01	0.01	0.02

Useful equations

$$A = \frac{Q}{N \cdot q}$$

$$V = 0.849 \times C \times R^{0.63} \times S^{0.54}$$

$$G^2 = \frac{P}{\mu \cdot Vol}$$

$$c = \frac{1 - e^{-k\bar{\epsilon}(H/B)}}{2k\bar{\epsilon}}$$

Q1-A

① Sedimentation process

1. The design of tank depended on SOR , d_w , d_p , Re number
2. There is no any filter media in the basin
3. The Geometric shape may be designing of rectangular or circular
4. Use to clarification the raw water after the coagulation - flocculation process.
5. there is no back washing water to cleaning the tanks
6. The sedimentation process yield to product the clarifier water + sludge

② Loop Network system

1. Hard work in design & construction
2. Homogeneous pressure
3. If the one pipe has been crushed the the next region feed by other pipe
4. There is no dead end zones in the loop system
5. More expensive

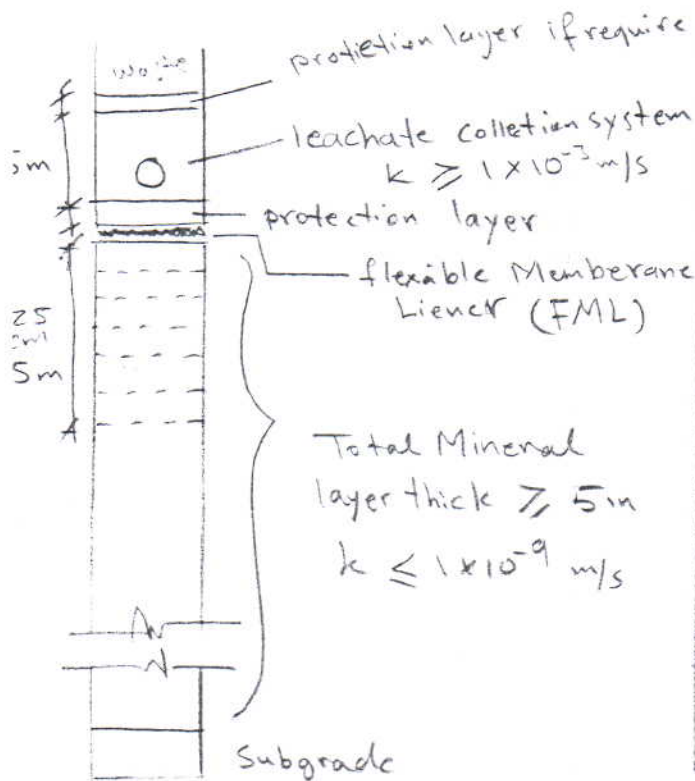
Filtration Process

1. The design of tank depends on filtration rate, surface area, Q
2. There are many types of materials that use as filter media in the basin
3. Usually rectangular volume.
4. use to filtering the water after sedimentation process
5. using the backwashing water to cleaning the filters.
6. The filtration process yield to filtered water.

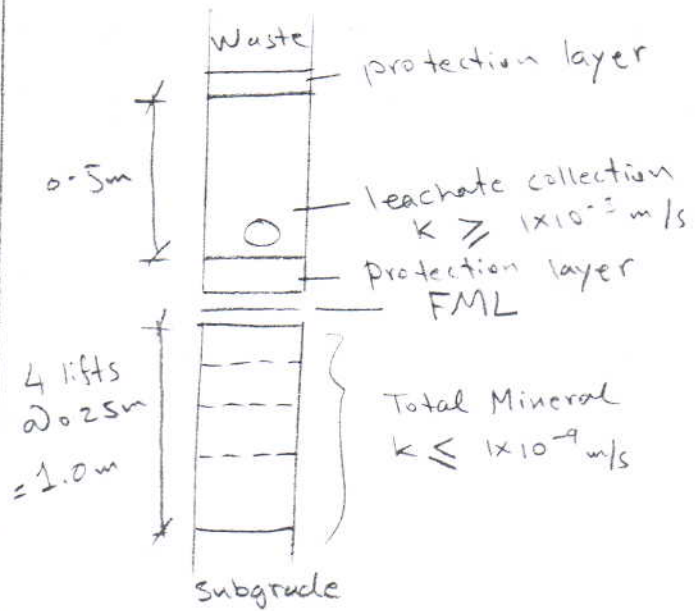
Tree Water system

1. More easy in design & construction methodes
2. Non-homogeneous pressure
3. If the hammer pheramy happen in one of pipe in the network that may be lead to incapacitate in the next region.
4. this network contains the dead end & the material can be sedimentate at the min. velocity
5. least expensive.

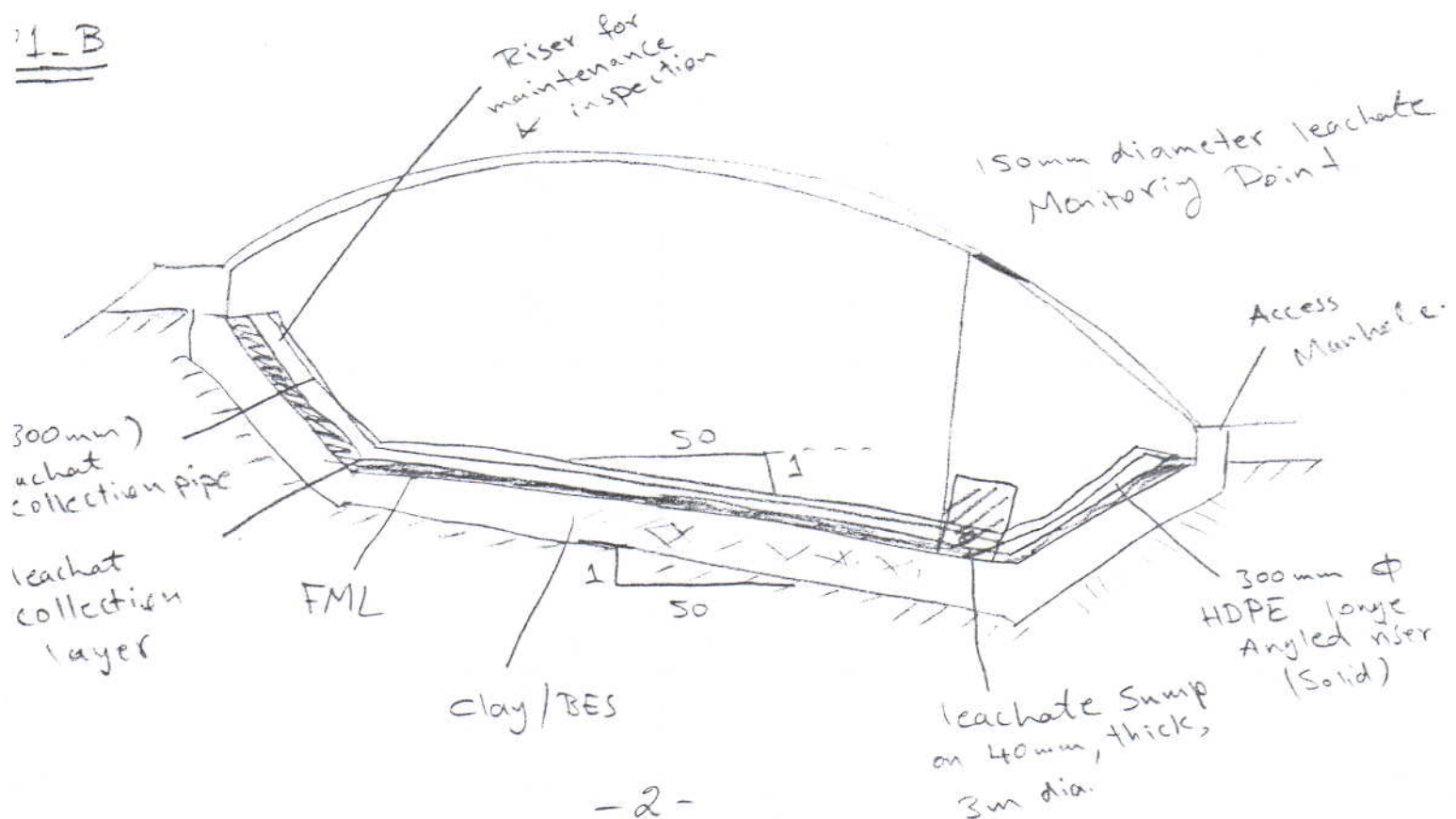
1 Lining System for Hazardous Waste Land fill (Option-1)



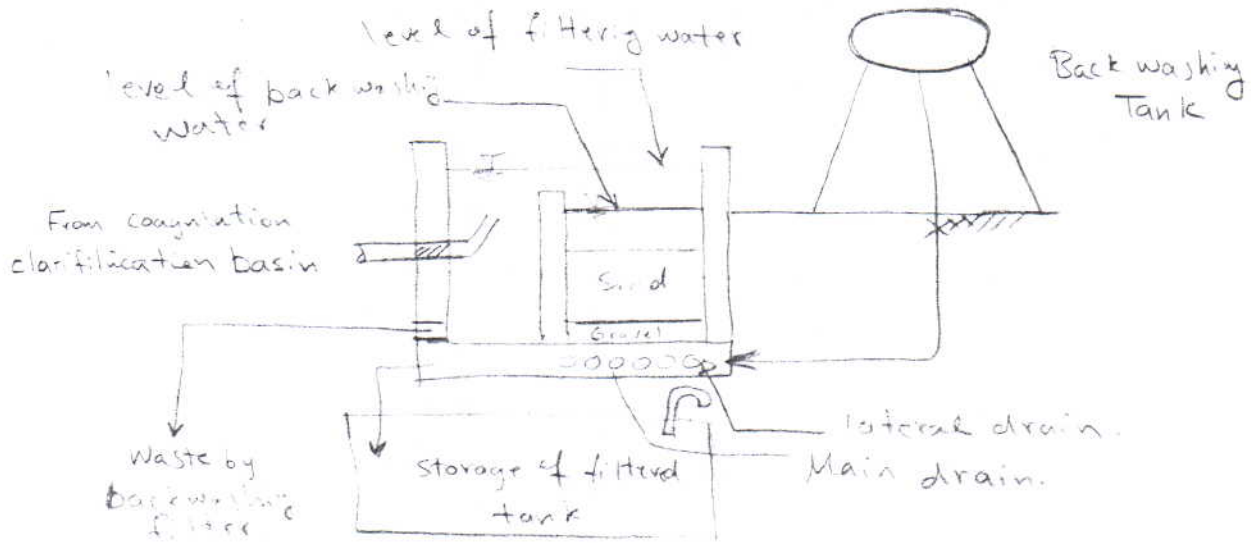
Lining system for Non-Hazardous biodegradable waste land fill



1-B



1B - (2)



2-2-A Solution

$$\textcircled{1} \quad \frac{d_1}{d_2} = \left(\frac{s_2 - s_w}{s_1 - s_w} \right)^{2/3} \Rightarrow d_2 = 0.5 \text{ mm for silica sand.}$$

For the anthracite

$$d_1 = 0.5 \left(\frac{2.6 - 1}{1.5 - 1} \right)^{2/3} = 1.1 \text{ mm}$$

For the ilmenite

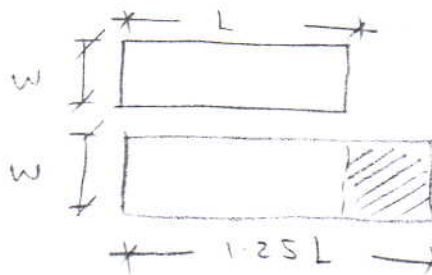
$$d_1 = 0.5 \left(\frac{2.6 - 1}{4.2 - 1} \right)^{2/3} = 0.3 \text{ mm}$$

$$\textcircled{2} \quad A_1 = W \cdot L$$

$$A_2 = 1.25 W \cdot L$$

Kawamura's formula

$$A = \frac{Q}{N \cdot g}$$



$$Q_{bw1} = 0.03 Q_1$$

$$Q_1 = \frac{Q_{bw1}}{0.03} = 33.33 Q_{bw1} \quad \text{--- (1)}$$

$$Q_2 = \frac{Q_{bw2}}{0.025} \quad \text{but } Q_{bw2} = 1.3 Q_{bw1}$$

$$\therefore Q_2 = \frac{1.3 Q_{bw1}}{0.025} = 52 Q_{bw1} \quad \text{--- (2)}$$

$$A = \frac{Q}{N \cdot q} \Rightarrow q = \frac{Q}{N \cdot A} \quad N_1 = 1, N_2 = 1$$

$$q_1 = \frac{Q_1}{N_1 (W \cdot L)} \quad , \quad q_2 = \frac{Q_2}{N_2 (1.25 W \cdot L)}$$

The filtration rate % After increasing the filter length

$$\frac{q_2}{q_1} = \frac{\frac{Q_2}{N_2 \cdot 1.25 W \cdot L}}{\frac{Q_1}{N_1 W \cdot L}} = \frac{52 Q_{bw1} / 1.25 W \cdot L}{33.33 Q_{bw1} / W \cdot L} = \frac{52}{33.33 \times 1.25} = 1.248$$

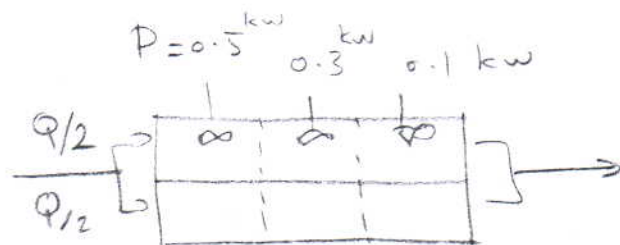
The increasing rate for filtration

$$\Rightarrow \left(\frac{q_2}{q_1} \times 100\% \right) - 100\%$$

$$124.8 - 100 = \boxed{24.8\%} \quad \text{معدل الزيادة في
المرشح إذا زاد طول
المرشح بمقدار (1.25)}$$

Q3

$$DT = 30 \text{ min} = 30 \times 60 = 1800 \text{ sec.}$$



dt for each basine = 10 min = 600 sec.

1- Find the flowrate ($Q/2$)

$$\frac{Q}{2} = \frac{Vol}{DT} \quad \therefore \quad G^2 = \frac{P}{k \cdot Vol}$$

$$\text{but } GT = G \times DT \Rightarrow G = \frac{GT}{DT} = \frac{1 \times 10^5}{30 \times 60} = 55.56 \text{ sec}^{-1}$$

$$G_{\text{Total}} = \frac{G_1 + 0.8 G_1 + 0.4 G_1}{3} \Rightarrow 55.56 = \frac{2.2}{3} G_1$$

$$\therefore G_1 = 75.76 \text{ sec}^{-1}$$

$$\Rightarrow Vol_1 = \frac{P_1}{k \times G_1^2} = \frac{0.5 \times 10^3}{1.3 \times 10^{-3} \times (75.76)^2} = \boxed{67.01 \text{ m}^3}$$

$$\Rightarrow G_2 = 0.8 G_1 = 60.61 \text{ s}^{-1} \Rightarrow Vol_2 = \frac{0.3 \times 10^3}{1.3 \times 10^{-3} \times (60.61)^2} = 61.79 \text{ m}^3$$

$$G_3 = 0.4 G_1 = 30.30 \text{ s}^{-1} \Rightarrow Vol_3 = \boxed{83.78 \text{ m}^3}$$

$$\frac{Q}{2} = \frac{Vol_1 + Vol_2 + Vol_3}{DT} \Rightarrow Q = 2 \times \frac{67.01 + 61.79 + 83.78}{30} = \boxed{14.172 \text{ m}^3/\text{min}}$$

$$\text{overall flowrate} = Q \times 2 = \boxed{20407.68 \text{ m}^3/\text{d}}$$

2- The concentration of Alum.

$$\text{quantity} = Q \times \text{Conc.} \Rightarrow \text{Conc.} = \frac{\text{quantity}}{Q} = \frac{120 \times 10^6 \text{ mg/d}}{20407.68 \text{ m}^3/\text{d}}$$

$$= 5880.13 \text{ mg/m}^3 = \boxed{5.88 \text{ mg/l}}$$

$$3- \text{Overall Surface Area} = \frac{2(V_1 + V_2 + V_3)}{3.5} = \frac{121,47}{3.5} = \boxed{125 \text{ m}^2}$$

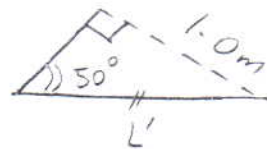
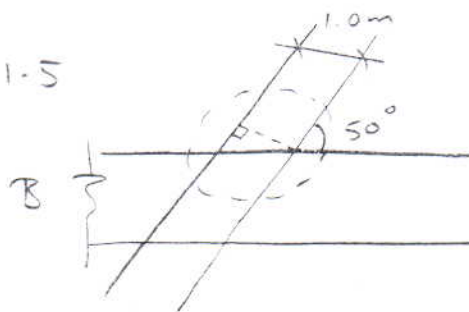
Q4

Solution:-

use F.S = 1.5

$$L.F = \frac{\text{Total loads}}{\text{Crushing strength}} \times F.S$$

↓
1.5



$$L' = \frac{1.0}{\sin 50} = 1.305 \text{ m}$$

Static load:

$$W = C \cdot \phi \cdot B^2$$

$$B_{\text{min}} = 1.5 \times \phi + 300$$

according to
ASTM

$$= 1.5 \times 600 + 300 = 1,200 \text{ mm}$$

$$C = \frac{1 - e^{-2kH(H/B)}}{2kH} = 1.20 \text{ m}$$

kH from table = 0.11

$$C = \frac{1 - e^{-2 \times 0.11 (2.5/1.2)}}{2 \times 0.11} = 1.671$$

$$\Rightarrow W = 1.671 \times 1920 \times (1.2)^2 = 4620.5 \text{ kg/m.l.}$$

↑
from Table

Non-Static load

$$B = 1.20 \text{ m} < L' = 1.3 \text{ m}$$

∵ $L' > B \Rightarrow$ ∵ long superficial loading

$$H/B \text{ ratio} = 2.083 \Rightarrow \text{superficial load factor} = 0.579$$

weight of water channel = 1500 kg/m

$$\frac{1500 \times 1.305}{1.20} = 1631.25 \text{ kg/m}$$

توزيل احماله الحمل باتجاه الانبوب

$$\Rightarrow \text{Non-Static Load} = 1631.25 \times 0.579 = 944.49 \text{ kg/m}$$

$$\Rightarrow \text{Total load} = 4620.5 + 944.49 = 5564.99 \approx 5565 \text{ kg/m}$$

$$\text{Load Factor } L.F = \frac{\text{Total load}}{\text{Crushing strength}} \times F.S = \frac{5565}{3500} \times 1.5 = 2.385$$

instruct the Class A-1 concrete cradle, L.F. = 2.8


 $P_A = 25 \text{ m}$

$$S = \frac{P_A - P_B}{L} = \frac{25 - 17.75}{300} = 0.02416$$

by chart:

$$\Rightarrow V = 1.85 \text{ m/s} \quad \Rightarrow V_{\text{Range}} = (0.6 - 1.20) \text{ m/s}$$
$$Q = 0.082 \text{ m}^3/\text{s} \quad \underline{\underline{0.1k}}$$
$$= 7084.8 \text{ m}^3/\text{d}$$

$$\Rightarrow \text{number of pop.} = \frac{Q}{q} = \frac{7084.8 \times 10^3}{250} = 28339 \text{ person}$$

Hazen William

$= 1.98 \text{ m/s}$ out of the Range of design
($0.6 - 1.2$) m/s

- 7 -

For Re-design

Use Av. Velocity $V_{av} = 0.90 \text{ m}$

But the Q which service the city is equal to

$$Q = 0.082 \text{ m}^3/\text{s} \quad \& \quad V = 0.90 \text{ m/s}$$

$$\therefore \text{New dia of pipe} = \frac{Q}{V} = \frac{0.082}{0.9} \text{ m/s}$$

$$\approx 91 \text{ mm} \approx 9.1 \text{ cm}$$

$$\text{USE } 10 \text{ cm} \Rightarrow V_{av} = 0.90 \text{ m}$$

USE

$$V = 0.6 \text{ m/s} \Rightarrow d = 136 \text{ mm}$$

$$V = 1.2 \text{ m/s} \Rightarrow d = 68 \text{ mm}$$